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Abstract

Optimized stellarator configurations will need to demonstrate desirable physics properties while simultaneously exhibiting a practical set of discrete coils, along with additional infrastructure and support structures necessary for the robust and stable operation of the device. The work here explores the use of the stellarator optimization suite, STELLOPT, to search for configurations that are predicted to have 1) better ideal MHD ballooning stability limits, and 2) improved coil winding surfaces that may lead to coils with improved engineering metrics. The ideal MHD ballooning stability calculation, based on a calculation requiring only the VMEC output data, is provided by COBRA. A rapid calculation of the coil winding surface current potential, the residual |Bnorm| error and a measure of the distances between coils, is provided by REGCOIL. By using metrics from both codes in the STELLOPT cost function, configurations with improved winding surfaces (reduced |Bnorm| error) and higher stability limits are found. Initial results of the optimization of quasi-symmetric stellarator configurations and candidate coil metrics will be shown.

Optimization Procedure

• Non-Linear Optimization procedure that adjusts the Fourier spectrum of the plasma boundary and coil winding surface to find configurations with improved characteristics

Configuration Comparisons

QHS

Improving ideal ballooning stability limits and coil winding surfaces with STELLOPT

• Standard configuration of the Helically Symmetric Experiment (HSX) • Straight-line B-field spectrum dominated by (n,m) = (4,1) helical component • Vacuum transform from 1.05 – 1.10 • Bootstrap current *unwinds/lowers* the transform • Mercier stability improves with beta due to deeper well • Ideal ballooning stability limit between β =1.5% - 1.7% (with or without bootstrap current)



Without Bootstrap Current

With Self-Consistent Bootstrap Current

- β = 0 %, Itor = 7.6301e-14 kA $\beta = 0 \%$ β = 0.73986 %, Itor = 4.3871 kA $\beta = 0.73986 \%$ — β = 1.5023 %, Itor = 8.5302 kA $\beta = 1.5023$ % $\beta = 2.2891$ % ltor = 12.6232 *β* = 2.2891 % $0.9 \parallel - \beta = 0 \%$ β = 0.73986 % --- β = 1.5023 % *β* = 2.2891 % 0.2 0.4 0.6 0.8 0.2 0.4 0.6 0.8 02 0.4 0.6 0.8 $\rho = \sqrt{\psi_{tor}/\psi_{tor,LCFS}}$ $ho = \sqrt{\psi_{tor}/\psi_{tor,LCFS}}$ $\rho = \sqrt{\psi_{tor}/\psi_{tor,LCFS}}$ Mercier Stability





2000

β = 0 %, Itor = 3.6795e-14 kA

 $\beta = 1.6256$ %, Itor = 11.8029 kA

β = 4.2931 %, Itor = 34.2197 kA

0.2

Ballooning Growth Rates

 β = 3.3666 %, Itor = 23.3656 kA

 $ho= rac{0.4}{\sqrt{\psi_{tor}/\psi_{tor,LCFS}}} \ 0.8$



Well (10%)

• A 'high iota' configuration of the Helically Symmetric Experiment (HSX) with increased well depth (stability) • Vacuum transform from 1.25 – 1.35 • Ideal ballooning stability limit @ β = 2.5% (without bootstrap current) or >3.3% (with bootstrap current)



 $\beta = 0 \%$

 $\beta = 3.1637 \%$

β = 1.5353 %

β = 1.7619 %

WISTELL CANDIDATES

- Several preliminary configurations are under consideration for in-depth analysis and (possible) optimization. $\frac{10}{7}\approx 1.43$
- Self-consistent bootstrap current included in this analysis
- All configuration are ballooning unstable above $\beta = 1.1\%$
- Mercier criterion convergence needs to be confirmed.
- Configurations have either 4 or 5 field periods







1.1

Plasma Profiles

• 2-Species (Hydrogen) plasma Temperature: $T_i(s) = T_e(s) = T_0 (1 - s)$ Density profiles $n_i(s) = n_e(s) = 7 \times 10^{19} (1 - s^5) m^{-3}$ Radial Coordinate: $s \equiv \psi/\psi_{LCFS}$, $\psi_{LCFS} = PHIEDGE$, $g^{ss} = |\overrightarrow{\nabla s}|^2$ • Bootstrap current

Analytic expression of bootstrap current in the collisionless limit¹ Self-consistent profiles calculated via an internal loop in STELLOPT

Mercier Criterion

Mercier stability is given by ^{2,3} :	$D_M = D_S + D_W + D_I + D_G \ge 0$
 Stabalizing shear term: 	$D_S \frac{t^2 \pi^2}{s} = \frac{(\Psi'' \Phi')^2}{4}$
• Well (or hill) term:	$D_W \ \frac{t^2 \pi^2}{s} = \int \int g d\theta d\zeta \ \frac{B^2}{g^{ss}} \frac{dp}{ds} \times \left(V'' - \frac{dp}{ds} \int \int g \frac{d\theta d\zeta}{B^2} \right)$
 Net current: 	$D_I \frac{t^2 \pi^2}{s} = \left[\int \int g \frac{d\theta d\zeta}{a^{ss}} \frac{B^2}{a^{ss}} \Psi'' I' - (\Psi'' \Phi') \int \int g \frac{(J \cdot B) d\theta d\zeta}{a^{ss}} \right]$

• Net current:

• Geodesic curvature:

Ballooning Stability

• Ideal ballooning mode growth rates are rapidly and accurately calculated using VMEC coordinates⁴

 $\alpha(s,\theta_{\nu},\zeta_{\nu}) = \theta_{\nu} + \lambda(s,\theta_{\nu},\zeta_{\nu}) - t\zeta_{\nu}$ $\left(\vec{B} \cdot \nabla\right) \left[\frac{|\nabla \alpha|^2}{R^2} \left(\vec{B} \cdot \nabla\right) \right] F + \left(\frac{R_0}{\alpha}\right)^2 \frac{\beta_0 p'}{\Psi'^2} \kappa_s F = \gamma^2 \frac{|\nabla \alpha|^2}{R^2} F$

 $D_G \frac{t^2 \pi^2}{s} = \left[\int \int g \frac{(J \cdot B) d\theta d\zeta}{q^{ss}} \right]^2 - \left[\int \int g \frac{(J \cdot B)^2 d\theta d\zeta}{q^{ss} B^2} \right] \int \int g \frac{B^2 d\theta d\zeta}{q^{ss}}$

Coil Winding Surface

• Normal component of B on the plasma surface: $\chi_B^2 = \int d^2 a B_{\perp}^2$ • Current density on the winding surface is given by $\vec{K} = \hat{n} \times \nabla \Phi$ • Surface-average-squared current density $K^2 = |\mathbf{K}|^2$ on the winding surface: $\chi_K^2 = \int d^2 a' K^2$ • REGCOIL⁵ finds the current potential, Φ , on the winding surface which minimizes: $\chi^2 = \chi_B^2 + \lambda \chi_K^2$ • Regularization parameter, λ : Large regularization leads to less complicated current potential contours ('less harmonic content'), but χ^2_B increases

• REGCOIL cost function targets available for STELLOPT (**bold** indicates targets used in this work)

 $\kappa_{MAX}, \kappa_{RMS}, \chi_{\kappa}^2$ $\chi_B^2, B_{\perp}(\theta, \zeta), max(B_{\perp})$ Minimum distance between plasma and winding surface Volume (plasma, winding surface, or difference)

Surface area (plasma, winding surface, or difference)

Prior to Optimization

Ballooning stability limit: $\beta < 0.7\%$



After Optimization

Ballooning stability raised to $\beta \cong 0.9\%$ β = 0.84122 % β = 0.90233 % 1.15

 $\rho = \frac{0.5}{\sqrt{\psi_{tor}/\psi_{tor,LCFS}}}$

 $\rho = \sqrt{\frac{0.5}{\psi_{tor}/\psi_{tor,LCFS}}}$



Balloonir

β=1.2% with

6 coils / fp

g Growth Rates

Coil Metrics (Single filament model)

Coil-to-coil distance (min): 16.5 cm		6
Coil length (avg): 3.76 m	Coil length (max): 3.89 m	5
Toroidal extent (avg): 0.348 rad (20 °)	Toroidal extent (max): 0.387 [rad] (22 °)	MEC
Curvature (mean arclength): 2.97 m ⁻¹	Curvature (max arclength): 12.1 m ⁻¹	θ_V

• Discrete coils produce a noticeable coil ripple on inboard low-field side • An increase in the predicted growth rates is also observed

|B| on LCFS with |B| on LCFS with 6 coils / field period "Ideal current sheet" Ballooning Growth Rates β =1.2% with "Ideal curren Φ_{VMEC} Φ_{VMEC}

 $0.2
ho = rac{0.4}{\sqrt{\psi_{tor}/\psi_{tor,LCFS}}} rac{0.8}{0.8}$



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• Simultaneous optimization for ballooning stability and coils metrics on a winding surface is feasible in STELLOPT

• Other metrics (Γ_{c} , turbulence, etc.) can be included in the standard way with STELLOPT

• Can be adapted to work for permanent magnet solutions

• Coils can be further improved (reduced coil ripple, improved metrics) with FOCUS

• All six configurations are under analysis

